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# A New Keynesian Monetary Model

## The Ireland's (2004) model

[Ireland, P.N. (2004), "Money's role in the monetary business cycle",

*Journal of Money, credit & Banking*, 36(6), 969-983]

*Nota: otra versión simple de presentar un modelo monetario neo-keynesiano puede verse en el capítulo 3 del libro **Monetary Policy, Inflation, and the Business Cycle**, de Jordi Galí, en Princeton University Press, 2008.*

## 1. An Optimizing IS-LM-PC Specification

### 1.1 Overview

Here, the models of Ireland (1997) and McCallum and Nelson (1999) are modified to focus on the role of money in the monetary business cycle. The economy consists of a representative household, a representative finished goods-producing firm, a continuum of intermediate goods-producing firms indexed by  $i \in [0, 1]$ , and a monetary authority. During each period  $t = 0, 1, 2, \dots$ , each intermediate goods-producing firm produces a distinct, perishable intermediate good. Hence, intermediate goods may also be indexed by  $i \in [0, 1]$ , where firm  $i$  produces good  $i$ . The model features enough symmetry, however, to allow the analysis to focus on the behavior of a representative intermediate goods-producing firm, identified by the generic index  $i$ .

## 1.2 The Representative Household

The representative household enters period  $t$  with money  $M_{t-1}$  and bonds  $B_{t-1}$ . At the beginning of the period, the household receives a lump-sum nominal transfer  $T_t$  from the monetary authority. Next, the household's bonds mature, providing  $B_{t-1}$  additional units of money. The household uses some of this money to purchase  $B_t$  new bonds at nominal cost  $B_t/r_t$ , where  $r_t$  denotes the gross nominal interest rate between  $t$  and  $t + 1$ .

The household supplies  $h_t(i)$  units of labor to each intermediate goods-producing firm  $i \in [0, 1]$ , for a total of

$$h_t = \int_0^1 h_t(i) di$$

during period  $t$ . The household is paid at the nominal wage rate  $W_t$ . The household consumes  $c_t$  units of the finished good, purchased at the nominal price  $P_t$  from the representative finished goods-producing firm.

At the end of period  $t$ , the household receives nominal profits  $D_t(i)$  from each intermediate goods-producing firm  $i \in [0, 1]$ , for a total of

$$D_t = \int_0^1 D_t(i) di.$$

The household then carries  $M_t$  units of money into period  $t + 1$ , subject to the budget constraint

$$\frac{M_{t-1} + T_t + B_{t-1} + W_t h_t + D_t}{P_t} \geq c_t + \frac{B_t/r_t + M_t}{P_t}. \quad (1)$$

The household's preferences are described by the expected utility function

$$E \sum_{t=0}^{\infty} \beta^t a_t \{u[c_t, (M_t/P_t)/e_t] - \eta h_t\},$$

where  $1 > \beta > 0$  and  $\eta > 0$ . The preference shocks  $a_t$  and  $e_t$  follow the autoregressive process

$$\ln(a_t) = \rho_a \ln(a_{t-1}) + \varepsilon_{at} \quad (2)$$

and

$$\ln(e_t) = (1 - \rho_e) \ln(e) + \rho_e \ln(e_{t-1}) + \varepsilon_{et}, \quad (3)$$

where  $1 > \rho_a > -1$ ,  $1 > \rho_e > -1$ ,  $e > 0$ , and the zero-mean, serially uncorrelated innovations  $\varepsilon_{at}$  and  $\varepsilon_{et}$  are normally distributed with standard deviations  $\sigma_a$  and  $\sigma_e$ .

Thus, the household chooses  $c_t$ ,  $h_t$ ,  $B_t$ , and  $M_t$  for all  $t = 0, 1, 2, \dots$ , to maximize its utility subject to the budget constraint (1) for all  $t = 0, 1, 2, \dots$ . Letting  $m_t = M_t/P_t$  denote real balances,  $\pi_t = P_t/P_{t-1}$  the inflation rate,  $w_t = W_t/P_t$  the real wage rate, and  $\lambda_t$  the nonnegative multiplier on (1), the first-order conditions for this problem are

$$a_t u_1(c_t, m_t/e_t) = \lambda_t, \quad (4)$$

$$\eta a_t = \lambda_t w_t, \quad (5)$$

$$\lambda_t = \beta r_t E_t(\lambda_{t+1}/\pi_{t+1}), \quad (6)$$

$$(a_t/e_t)u_2(c_t, m_t/e_t) = \lambda_t - \beta E_t(\lambda_{t+1}/\pi_{t+1}), \quad (7)$$

and (1) with equality for all  $t = 0, 1, 2, \dots$

### 1.3 The Representative Finished Goods-Producing Firm

During each period  $t = 0, 1, 2, \dots$ , the representative finished goods-producing firm uses  $y_t(i)$  units of each intermediate good  $i \in [0, 1]$ , purchased at nominal price  $P_t(i)$ , to manufacture  $y_t$  units of the finished good according to the constant-returns-to-scale technology described by

$$\left[ \int_0^1 y_t(i)^{(\theta-1)/\theta} di \right]^{\theta/(\theta-1)} \geq y_t,$$

where  $\theta > 1$ . Thus, the finished goods-producing firm chooses  $y_t(i)$  for all  $i \in [0, 1]$  to maximize its profits, given by

$$P_t \left[ \int_0^1 y_t(i)^{(\theta-1)/\theta} di \right]^{\theta/(\theta-1)} - \int_0^1 P_t(i) y_t(i) di,$$

for all  $t = 0, 1, 2, \dots$ . The first-order conditions for this problem are

$$y_t(i) = [P_t(i)/P_t]^{-\theta} y_t$$

for all  $i \in [0, 1]$  and  $t = 0, 1, 2, \dots$

Competition drives the finished goods-producing firm's profits to zero in equilibrium. This zero-profit condition implies that

$$P_t = \left[ \int_0^1 P_t(i)^{1-\theta} di \right]^{1/(1-\theta)}$$

for all  $t = 0, 1, 2, \dots$



## 1.4 The Representative Intermediate Goods-Producing Firm

During each period  $t = 0, 1, 2, \dots$ , the representative intermediate goods-producing firm hires  $h_t(i)$  units of labor from the representative household to manufacture  $y_t(i)$  units of intermediate good  $i$  according to the constant-returns-to-scale technology described by

$$z_t h_t(i) \geq y_t(i). \quad (8)$$

The aggregate technology shock  $z_t$  follows the autoregressive process

$$\ln(z_t) = (1 - \rho_z) \ln(z) + \rho_z \ln(z_{t-1}) + \varepsilon_{zt}, \quad (9)$$

where  $1 > \rho_z > -1$  and  $z > 0$ . The zero-mean, serially uncorrelated innovation  $\varepsilon_{zt}$  is normally distributed with standard deviation  $\sigma_z$ .

Since the intermediate goods substitute imperfectly for one another in producing the finished good, the representative intermediate goods-producing firm sells its output in a monopolistically competitive market; during each period  $t = 0, 1, 2, \dots$ , the intermediate goods-producing firm sets the nominal price  $P_t(i)$  for its output, subject to the requirement that it satisfy the representative finished goods-producing firm's demand. In addition, the intermediate goods-producing firm faces a quadratic cost of adjusting its nominal price, measured in terms of the finished good and given by

$$\frac{\phi}{2} \left[ \frac{P_t(i)}{\pi P_{t-1}(i)} - 1 \right]^2 y_t,$$

where  $\phi > 0$  and where  $\pi$  denotes the steady-state inflation rate.

The cost of price adjustment makes the intermediate goods-producing firm's problem dynamic; it chooses  $P_t(i)$  for all  $t = 0, 1, 2, \dots$  to maximize its total market value, given by

$$E \sum_{t=0}^{\infty} \beta^t \lambda_t [D_t(i)/P_t],$$

where  $\beta^t \lambda_t / P_t$  measures the marginal utility value to the representative household of an additional dollar in profits received during period  $t$  and where

$$\frac{D_t(i)}{P_t} = \left[ \frac{P_t(i)}{P_t} \right]^{1-\theta} y_t - \left[ \frac{P_t(i)}{P_t} \right]^{-\theta} \left( \frac{w_t y_t}{z_t} \right) - \frac{\phi}{2} \left[ \frac{P_t(i)}{\pi P_{t-1}(i)} - 1 \right]^2 y_t \quad (10)$$

for all  $t = 0, 1, 2, \dots$ . The first-order conditions for this problem are

$$\begin{aligned}
 0 = & (1 - \theta)\lambda_t \left[ \frac{P_t(i)}{P_t} \right]^{-\theta} \left( \frac{y_t}{P_t} \right) + \theta\lambda_t \left[ \frac{P_t(i)}{P_t} \right]^{-\theta-1} \left( \frac{y_t w_t}{z_t P_t} \right) \\
 & - \phi\lambda_t \left[ \frac{P_t(i)}{\pi P_{t-1}(i)} - 1 \right] \left[ \frac{y_t}{\pi P_{t-1}(i)} \right] \\
 & + \beta\phi E_t \left\{ \lambda_{t+1} \left[ \frac{P_{t+1}(i)}{\pi P_t(i)} - 1 \right] \left[ \frac{y_{t+1} P_{t+1}(i)}{\pi P_t(i)^2} \right] \right\}
 \end{aligned} \tag{11}$$

for all  $t = 0, 1, 2, \dots$

## 1.5 The Monetary Authority

The monetary authority conducts monetary policy by adjusting the nominal interest rate  $r_t$  in response to deviations of output  $y_t$ , inflation  $\pi_t$ , and money growth

$$\mu_t = M_t/M_{t-1} \quad (12)$$

from their steady-state values  $y$ ,  $\pi$ , and  $\mu$  according to the policy rule

$$\ln(r_t/r) = \rho_r \ln(r_{t-1}/r) + \rho_y \ln(y_{t-1}/y) + \rho_\pi \ln(\pi_{t-1}/\pi) + \rho_\mu \ln(\mu_{t-1}/\mu) + \varepsilon_{rt}, \quad (13)$$

where  $r$  is the steady-state value of  $r_t$  and where the zero-mean, serially uncorrelated innovation  $\varepsilon_{rt}$  is normally distributed with standard deviation  $\sigma_r$ .

## 1.6 Symmetric Equilibrium

In a symmetric equilibrium, all intermediate goods-producing firms make identical decisions, so that  $y_t(i) = y_t$ ,  $h_t(i) = h_t$ ,  $P_t(i) = P_t$ , and  $d_t(i) = D_t(i)/P_t = D_t/P_t = d_t$  for all  $i \in [0, 1]$  and  $t = 0, 1, 2, \dots$ . In addition, the market-clearing conditions  $M_t = M_{t-1} + T_t$  and  $B_t = B_{t-1} = 0$  must hold for all  $t = 0, 1, 2, \dots$ .

After imposing these conditions (1)-(13) become

$$y_t = c_t + \frac{\phi}{2} \left( \frac{\pi_t}{\pi} - 1 \right)^2 y_t, \quad (1)$$

$$\ln(a_t) = \rho_a \ln(a_{t-1}) + \varepsilon_{at}, \quad (2)$$

$$\ln(e_t) = (1 - \rho_e) \ln(e) + \rho_e \ln(e_{t-1}) + \varepsilon_{et}, \quad (3)$$

$$a_t u_1(c_t, m_t/e_t) = \lambda_t, \quad (4)$$

$$\eta a_t = \lambda_t w_t, \quad (5)$$

$$\lambda_t = \beta r_t E_t(\lambda_{t+1}/\pi_{t+1}), \quad (6)$$

$$(a_t/e_t)u_2(c_t, m_t/e_t) = \lambda_t - \beta E_t(\lambda_{t+1}/\pi_{t+1}), \quad (7)$$

$$y_t = z_t h_t, \quad (8)$$

$$\ln(z_t) = (1 - \rho_z) \ln(z) + \rho_z \ln(z_{t-1}) + \varepsilon_{zt}, \quad (9)$$

$$d_t = y_t - w_t h_t - \frac{\phi}{2} \left( \frac{\pi_t}{\pi} - 1 \right)^2 y_t, \quad (10)$$

$$0 = (1 - \theta)\lambda_t + \theta\lambda_t \left( \frac{w_t}{z_t} \right) - \phi\lambda_t \left( \frac{\pi_t}{\pi} - 1 \right) \left( \frac{\pi_t}{\pi} \right) \quad (11)$$

$$+ \beta\phi E_t \left[ \lambda_{t+1} \left( \frac{\pi_{t+1}}{\pi} - 1 \right) \left( \frac{y_{t+1}}{y_t} \right) \left( \frac{\pi_{t+1}}{\pi} \right) \right],$$

$$m_{t-1}\mu_t = m_t\pi_t, \quad (12)$$

and

$$\ln(r_t/r) = \rho_r \ln(r_{t-1}/r) + \rho_y \ln(y_{t-1}/y) + \rho_\pi \ln(\pi_{t-1}/\pi) + \rho_\mu \ln(\mu_{t-1}/\mu) + \varepsilon_{rt}. \quad (13)$$

These 13 equations determine equilibrium values for the 13 variables  $y_t$ ,  $\pi_t$ ,  $m_t$ ,  $r_t$ ,  $c_t$ ,  $h_t$ ,  $w_t$ ,  $d_t$ ,  $\lambda_t$ ,  $\mu_t$ ,  $a_t$ ,  $e_t$ , and  $z_t$ .

Use (4), (5), (8), and (10) to eliminate  $\lambda_t$ ,  $w_t$ ,  $h_t$ , and  $d_t$ . Then the system can be written more compactly as



$$y_t = c_t + \frac{\phi}{2} \left( \frac{\pi_t}{\pi} - 1 \right)^2 y_t, \quad (1)$$

$$\ln(a_t) = \rho_a \ln(a_{t-1}) + \varepsilon_{at}, \quad (2)$$

$$\ln(e_t) = (1 - \rho_e) \ln(e) + \rho_e \ln(e_{t-1}) + \varepsilon_{et}, \quad (3)$$

$$a_t u_1(c_t, m_t/e_t) = \beta r_t E_t [a_{t+1} u_1(c_{t+1}, m_{t+1}/e_{t+1}) / \pi_{t+1}], \quad (6)$$

$$r_t u_2(c_t, m_t/e_t) = (r_t - 1) e_t u_1(c_t, m_t/e_t), \quad (7)$$

$$\ln(z_t) = (1 - \rho_z) \ln(z) + \rho_z \ln(z_{t-1}) + \varepsilon_{zt}, \quad (9)$$

$$\theta - 1 = \theta \left[ \frac{\eta}{z_t u_1(c_t, m_t/e_t)} \right] - \phi \left( \frac{\pi_t}{\pi} - 1 \right) \left( \frac{\pi_t}{\pi} \right) \quad (11)$$

$$+ \beta \phi E_t \left\{ \left[ \frac{a_{t+1} u_1(c_{t+1}, m_{t+1}/e_{t+1})}{a_t u_1(c_t, m_t/e_t)} \right] \left( \frac{\pi_{t+1}}{\pi} - 1 \right) \left( \frac{y_{t+1}}{y_t} \right) \left( \frac{\pi_{t+1}}{\pi} \right) \right\},$$

$$m_{t-1} \mu_t = m_t \pi_t, \quad (12)$$

and

$$\ln(r_t/r) = \rho_r \ln(r_{t-1}/r) + \rho_y \ln(y_{t-1}/y) + \rho_\pi \ln(\pi_{t-1}/\pi) + \rho_\mu \ln(\mu_{t-1}/\mu) + \varepsilon_{rt}. \quad (13)$$

These 9 equations determine equilibrium values for the 9 variables  $y_t$ ,  $\pi_t$ ,  $m_t$ ,  $r_t$ ,  $c_t$ ,  $\mu_t$ ,  $a_t$ ,  $e_t$ , and  $z_t$ .

## 1.7 The Steady State

In the absence of shocks, the economy converges to a steady state, in which  $y_t = y$ ,  $\pi_t = \pi$ ,  $m_t = m$ ,  $r_t = r$ ,  $c_t = c$ ,  $\mu_t = \mu$ ,  $a_t = a$ ,  $e_t = e$ , and  $z_t = z$ . The steady-state values  $a$ ,  $e$ , and  $z$  are determined by (2), (3), and (9). The steady-state value  $\pi$  is determined by (13).

The steady-state value  $r$  is determined by (6) as

$$r = \pi/\beta.$$

The steady-state value  $\mu$  is determined by (12) as

$$\mu = \pi.$$

The steady-state value  $c$  is determined by (1) as

$$c = y.$$

The steady-state values  $y$  and  $m$  are determined by (7) and (11):

$$ru_2(y, m/e) = (r - 1)eu_1(y, m/e)$$

and

$$u_1(y, m/e) = \left( \frac{\theta}{\theta - 1} \right) \left( \frac{\eta}{z} \right).$$

## 1.8 The Linearized System

The system consisting of (1)-(3), (6), (7), (9), and (11)-(13) can be log-linearized around the steady state in order to describe how the economy responds to shocks. Let  $\hat{y}_t = \ln(y_t/y)$ ,  $\hat{\pi}_t = \ln(\pi_t/\pi)$ ,  $\hat{m}_t = \ln(m_t/m)$ ,  $\hat{r}_t = \ln(r_t/r)$ ,  $\hat{c}_t = \ln(c_t/c)$ ,  $\hat{\mu}_t = \ln(\mu_t/\mu)$ ,  $\hat{a}_t = \ln(a_t/a)$ ,  $\hat{e}_t = \ln(e_t/e)$ , and  $\hat{z}_t = \ln(z_t/z)$ . The first-order Taylor approximations yield

$$\hat{y}_t = \hat{c}_t, \tag{1}$$

$$\hat{a}_t = \rho_a \hat{a}_{t-1} + \varepsilon_{at}, \tag{2}$$

$$\hat{e}_t = \rho_e \hat{e}_{t-1} + \varepsilon_{et}, \tag{3}$$

$$\begin{aligned} \hat{y}_t = & E_t \hat{y}_{t+1} - \omega_1(\hat{r}_t - E_t \hat{\pi}_{t+1}) + \omega_2(\hat{m}_t - E_t \hat{m}_{t+1}) \\ & - \omega_2(\hat{e}_t - E_t \hat{e}_{t+1}) + \omega_1(\hat{a}_t - E_t \hat{a}_{t+1}), \end{aligned} \tag{6}$$

$$\hat{m}_t = \gamma_1 \hat{y}_t - \gamma_2 \hat{r}_t + \gamma_3 \hat{e}_t, \quad (7)$$

$$\hat{z}_t = \rho_z \hat{z}_{t-1} + \varepsilon_{zt}, \quad (9)$$

$$\hat{\pi}_t = \left(\frac{\pi}{r}\right) E_t \hat{\pi}_{t+1} + \psi \left[ \left(\frac{1}{\omega_1}\right) \hat{y}_t - \left(\frac{\omega_2}{\omega_1}\right) \hat{m}_t + \left(\frac{\omega_2}{\omega_1}\right) \hat{e}_t - \hat{z}_t \right], \quad (11)$$

$$\hat{m}_{t-1} + \hat{\mu}_t = \hat{m}_t + \hat{\pi}_t, \quad (12)$$

and

$$\hat{r}_t = \rho_r \hat{r}_{t-1} + \rho_y \hat{y}_{t-1} + \rho_\pi \hat{\pi}_{t-1} + \rho_\mu \hat{\mu}_{t-1} + \varepsilon_{rt}, \quad (13)$$

where

$$\omega_1 = -\frac{u_1(y, m/e)}{yu_{11}(y, m/e)},$$

$$\omega_2 = -\frac{(m/e)u_{12}(y, m/e)}{yu_{11}(y, m/e)},$$

$$\gamma_1 = \left( \frac{yr\omega_2}{m\omega_1} + \frac{r-1}{\omega_1} \right) \gamma_2,$$

$$\gamma_2 = \frac{r}{(r-1)(m/e)} \left[ \frac{u_2(y, m/e)}{(r-1)eu_{12}(y, m/e) - ru_{22}(y, m/e)} \right],$$

$$\gamma_3 = 1 - (r-1)\gamma_2,$$

and

$$\psi = \frac{\theta - 1}{\phi}.$$

Equation (6) is the IS curve, equation (7) is the LM curve, equation (11) is the Phillips curve, and equation (13) is the policy rule. Use (1) to eliminate  $c_t$ , and rewrite the system as

$$\hat{a}_t = \rho_a \hat{a}_{t-1} + \varepsilon_{at}, \quad (2)$$

$$\hat{e}_t = \rho_e \hat{e}_{t-1} + \varepsilon_{et}, \quad (3)$$

$$\begin{aligned} \hat{y}_t = & E_t \hat{y}_{t+1} - \omega_1 (\hat{r}_t - E_t \hat{\pi}_{t+1}) + \omega_2 (\hat{m}_t - E_t \hat{m}_{t+1}) \\ & - \omega_2 (1 - \rho_e) \hat{e}_t + \omega_1 (1 - \rho_a) \hat{a}_t, \end{aligned} \quad (6)$$

$$\hat{m}_t = \gamma_1 \hat{y}_t - \gamma_2 \hat{r}_t + \gamma_3 \hat{e}_t, \quad (7)$$

$$\hat{z}_t = \rho_z \hat{z}_{t-1} + \varepsilon_{zt}, \quad (9)$$

$$\hat{\pi}_t = \left(\frac{\pi}{r}\right) E_t \hat{\pi}_{t+1} + \psi \left[ \left(\frac{1}{\omega_1}\right) \hat{y}_t - \left(\frac{\omega_2}{\omega_1}\right) \hat{m}_t + \left(\frac{\omega_2}{\omega_1}\right) \hat{e}_t - \hat{z}_t \right], \quad (11)$$



$$\hat{m}_{t-1} + \hat{\mu}_t = \hat{m}_t + \hat{\pi}_t, \quad (12)$$

and

$$\hat{r}_t = \rho_r \hat{r}_{t-1} + \rho_y \hat{y}_{t-1} + \rho_\pi \hat{\pi}_{t-1} + \rho_\mu \hat{\mu}_{t-1} + \varepsilon_{rt}. \quad (13)$$

**A simplified version of the Ireland's (2004) model:**

$$U \left( c_t, \underbrace{\frac{M_{t+1}}{P_t} \frac{1}{e_t}}_{m_{t+1}} \right) = \frac{\left[ c_t (m_{t+1} / e_t)^\varepsilon \right]^{1-\sigma} - 1}{1-\sigma}$$

Under this utility function the structural parameters are:

$$\varpi_1 = 1/\sigma; \quad \varpi_2 = \theta \frac{1-\sigma}{\sigma}; \quad \gamma_1 = 1; \quad \gamma_2 = 1/(r-1); \quad \gamma_3 = 0;$$

Let the following equation be a simple Taylor rule:

$$\hat{r}_t = \rho_y \hat{y}_t + \rho_\pi \hat{\pi}_t + \varepsilon_{rt}$$

If  $\sigma=1$ , then,

$$\begin{bmatrix} 1 + \rho_y & \rho_\pi \\ -\frac{\theta - 1}{\phi} & 1 \end{bmatrix} \begin{bmatrix} \hat{y}_t \\ \hat{\pi}_t \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & \beta \end{bmatrix} \begin{bmatrix} E_t \hat{y}_{t+1} \\ E_t \hat{\pi}_{t+1} \end{bmatrix} + \begin{bmatrix} -1 & 0 & 1 - \rho_a & 0 \\ 0 & 0 & 0 & -\frac{\theta - 1}{\phi} \end{bmatrix} \begin{bmatrix} \varepsilon_{rt} \\ \hat{e}_t \\ \hat{a}_t \\ \hat{z}_t \end{bmatrix}$$

where we have assumed that the steady state of the structural shocks is zero.

The solution for the system of equations described above is:

$$\begin{bmatrix} \hat{y}_t \\ \hat{\pi}_t \end{bmatrix} = \begin{bmatrix} \Phi_1 & \Phi_2 & \Phi_3 \\ \Psi_1 & \Psi_2 & \Psi_3 \end{bmatrix} \begin{bmatrix} \hat{z}_t \\ \hat{a}_t \\ \varepsilon_{rt} \end{bmatrix}$$

$$\text{where } \Phi_1 = \frac{\left( C_{21} + \frac{(1 - A_{22}\rho_z)}{A_{12}\rho_z} C_{11} \right)}{\left[ \frac{(1 - A_{22}\rho_z)(1 - A_{11}\rho_z)}{A_{12}\rho_z} - A_{21}\rho_z \right]}; \quad \Psi_1 = \frac{(1 - A_{11}\rho_z)}{A_{12}\rho_z} \Phi_1 - \frac{C_{11}}{A_{12}\rho_z}$$

$$\Phi_2 = \frac{\left( C_{22} + \frac{(1 - A_{22}\rho_a)}{A_{12}\rho_a} C_{12} \right)}{\left[ \frac{(1 - A_{22}\rho_a)(1 - A_{11}\rho_a)}{A_{12}\rho_a} - A_{21}\rho_a \right]}; \quad \Psi_2 = \frac{(1 - A_{11}\rho_a)}{A_{12}\rho_a} \Phi_2 - \frac{C_{12}}{A_{12}\rho_a}$$

$$\Phi_3 = \frac{\left( C_{23} + \frac{(1 - A_{22}\rho_{\varepsilon_r})}{A_{12}\rho_{\varepsilon_r}} C_{13} \right)}{\left[ \frac{(1 - A_{22}\rho_{\varepsilon_r})(1 - A_{11}\rho_{\varepsilon_r})}{A_{12}\rho_{\varepsilon_r}} - A_{21}\rho_{\varepsilon_r} \right]}; \quad \Psi_3 = \frac{(1 - A_{11}\rho_{\varepsilon_r})}{A_{12}\rho_{\varepsilon_r}} \Phi_3 - \frac{C_{13}}{A_{12}\rho_{\varepsilon_r}}$$

where  $A_{ij}$  y  $C_{ik}$  are the elements of the following matrices:

$$A = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} = \begin{bmatrix} 1 + \rho_y & \rho_\pi \\ -\frac{\theta - 1}{\phi} & 1 \end{bmatrix}^{-1} \begin{bmatrix} 1 & 1 \\ 0 & \beta \end{bmatrix}$$
$$C = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \end{bmatrix} = \begin{bmatrix} 1 + \rho_y & \rho_\pi \\ -\frac{\theta - 1}{\phi} & 1 \end{bmatrix}^{-1} \begin{bmatrix} 0 & 1 - \rho_a & -1 \\ -\frac{\theta - 1}{\phi} & 0 & 0 \end{bmatrix}$$

## Impulse-response functions:

Given the following stochastic processes for structural shocks:

$$\begin{aligned}\hat{z}_t &= \rho_z \hat{z}_{t-1} + \varepsilon_{zt} \\ \hat{a}_t &= \rho_a \hat{a}_{t-1} + \varepsilon_{at} \\ \varepsilon_{r,t} &= \rho_{\varepsilon_r} \varepsilon_{r,t-1} + u_t\end{aligned}$$

it is easy to derive the impulse-response functions, using the following expressions:

$$\begin{aligned}\hat{y}_t &= \Phi_1 \sum_{j=0}^{\infty} \rho_z^j \varepsilon_{z,t-j} + \Phi_2 \sum_{j=0}^{\infty} \rho_a^j \varepsilon_{a,t-j} + \Phi_3 \sum_{j=0}^{\infty} \rho_{\varepsilon_r}^j u_{t-j} \\ \hat{\pi}_t &= \Psi_1 \sum_{j=0}^{\infty} \rho_z^j \varepsilon_{z,t-j} + \Psi_2 \sum_{j=0}^{\infty} \rho_a^j \varepsilon_{a,t-j} + \Psi_3 \sum_{j=0}^{\infty} \rho_{\varepsilon_r}^j u_{t-j}\end{aligned}$$

## Variance decomposition of forecast errors:

Given the following expressions:

$$\hat{y}_t = \Phi_1 \sum_{j=0}^{\infty} \rho_z^j \varepsilon_{z,t-j} + \Phi_2 \sum_{j=0}^{\infty} \rho_a^j \varepsilon_{a,t-j} + \Phi_3 \sum_{j=0}^{\infty} \rho_{\varepsilon_r}^j u_{t-j}$$

$$\hat{\pi}_t = \Psi_1 \sum_{j=0}^{\infty} \rho_z^j \varepsilon_{z,t-j} + \Psi_2 \sum_{j=0}^{\infty} \rho_a^j \varepsilon_{a,t-j} + \Psi_3 \sum_{j=0}^{\infty} \rho_{\varepsilon_r}^j u_{t-j}$$

it can be obtained, for  $n > 0$ :

$$\hat{y}_{t+n} - E_t \hat{y}_{t+n} = \Phi_1 \sum_{j=0}^{n-1} \rho_z^j \varepsilon_{z,t+n-j} + \Phi_2 \sum_{j=0}^{n-1} \rho_a^j \varepsilon_{a,t+n-j} + \Phi_3 \sum_{j=0}^{n-1} \rho_{\varepsilon_r}^j u_{t+n-j}$$

$$\hat{\pi}_{t+n} - E_t \hat{\pi}_{t+n} = \Psi_1 \sum_{j=0}^{n-1} \rho_z^j \varepsilon_{z,t+n-j} + \Psi_2 \sum_{j=0}^{n-1} \rho_a^j \varepsilon_{a,t+n-j} + \Psi_3 \sum_{j=0}^{n-1} \rho_{\varepsilon_r}^j u_{t+n-j}$$

$$\text{Var}(\hat{y}_{t+n} - E_t \hat{y}_{t+n}) = \frac{\Phi_1^2 \sigma_{\varepsilon_z}^2 (1 - \rho_z^{2n})}{1 - \rho_z^2} + \frac{\Phi_2^2 \sigma_{\varepsilon_a}^2 (1 - \rho_a^{2n})}{1 - \rho_a^2} + \frac{\Phi_3^2 \sigma_u^2 (1 - \rho_{\varepsilon_r}^{2n})}{1 - \rho_{\varepsilon_r}^2}$$

$$\text{Var}(\hat{\pi}_{t+1} - E_t \hat{\pi}_{t+n}) = \frac{\Psi_1^2 \sigma_{\varepsilon_z}^2 (1 - \rho_z^{2n})}{1 - \rho_z^2} + \frac{\Psi_2^2 \sigma_{\varepsilon_a}^2 (1 - \rho_a^{2n})}{1 - \rho_a^2} + \frac{\Psi_3^2 \sigma_u^2 (1 - \rho_{\varepsilon_r}^{2n})}{1 - \rho_{\varepsilon_r}^2}$$

Note that:  $\sum_{j=0}^{n-1} \rho^2 = \frac{(1 - \rho^{2n})}{1 - \rho^2}$ .



Therefore the variance decomposition of forecast errors for each variable will be:

$$D.V.E.P.(\hat{y}_{t+n}) = 100 \times \left( \frac{\frac{\Phi_1^2 \sigma_{\varepsilon_z}^2 (1 - \rho_z^{2n})}{1 - \rho_z^2}}{\text{Var}(\hat{y}_{t+n} - E_t \hat{y}_{t+n})}, \frac{\frac{\Phi_2^2 \sigma_{\varepsilon_a}^2 (1 - \rho_a^{2n})}{1 - \rho_a^2}}{\text{Var}(\hat{y}_{t+n} - E_t \hat{y}_{t+n})}, \frac{\frac{\Phi_3^2 \sigma_u^2 (1 - \rho_{\varepsilon_r}^{2n})}{1 - \rho_{\varepsilon_r}^2}}{\text{Var}(\hat{y}_{t+n} - E_t \hat{y}_{t+n})} \right),$$

$$D.V.E.P.(\hat{\pi}_{t+n}) = 100 \times \left( \frac{\frac{\Psi_1^2 \sigma_{\varepsilon_z}^2 (1 - \rho_z^{2n})}{1 - \rho_z^2}}{\text{Var}(\hat{\pi}_{t+n} - E_t \hat{\pi}_{t+n})}, \frac{\frac{\Psi_2^2 \sigma_{\varepsilon_a}^2 (1 - \rho_a^{2n})}{1 - \rho_a^2}}{\text{Var}(\hat{\pi}_{t+n} - E_t \hat{\pi}_{t+n})}, \frac{\frac{\Psi_3^2 \sigma_u^2 (1 - \rho_{\varepsilon_r}^{2n})}{1 - \rho_{\varepsilon_r}^2}}{\text{Var}(\hat{\pi}_{t+n} - E_t \hat{\pi}_{t+n})} \right).$$

## 2. Solving the Ireland's (2004) model

Let

$$f_t^0 = \begin{bmatrix} \hat{m}_t & \hat{r}_t & \hat{\mu}_t \end{bmatrix}',$$

$$s_t^0 = \begin{bmatrix} \hat{y}_{t-1} & \hat{m}_{t-1} & \hat{\pi}_{t-1} & \hat{r}_{t-1} & \hat{\mu}_{t-1} & \hat{y}_t & \hat{\pi}_t \end{bmatrix}',$$

and

$$v_t = \begin{bmatrix} \hat{a}_t & \hat{e}_t & \hat{z}_t & \varepsilon_{rt} \end{bmatrix}'.$$

Then (7), (12), and (13) can be written as

$$Af_t^0 = Bs_t^0 + Cv_t, \tag{14}$$

where  $A$  is  $3 \times 3$ ,  $B$  is  $3 \times 7$ , and  $C$  is  $3 \times 4$ .

$$A = \begin{bmatrix} 1 & \gamma_2 & 0 \\ 1 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix}; B = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & \gamma_1 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & -1 \\ \rho_y & 0 & \rho_\pi & \rho_r & \rho_\mu & 0 & 0 \end{bmatrix};$$

$$C = \begin{bmatrix} 0 & \gamma_3 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Equations (6) and (11) can be written as

$$DE_t s_{t+1}^0 + FE_t f_{t+1}^0 = Gs_t^0 + Hf_t^0 + Jv_t, \quad (15)$$

where  $D$  and  $G$  are  $7 \times 7$ ,  $F$  and  $H$  are  $7 \times 3$ , and  $J$  is  $7 \times 4$ .

$$D = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 1 & \omega_1 \\ 0 & 0 & 0 & 0 & 0 & 0 & \pi/r \\ 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 \end{bmatrix}; \quad F = \begin{bmatrix} -\omega_2 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$G = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & -\psi/\omega_1 & 1 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}; \quad H = \begin{bmatrix} -\omega_2 & \omega_1 & 0 \\ \psi(\omega_2/\omega_1) & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}; \quad J = \begin{bmatrix} -\omega_1(1-\rho_a) & \omega_2(1-\rho_e) & 0 & 0 \\ 0 & -\psi(\omega_2/\omega_1) & \psi & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Equations (2), (3), and (9) can be written as

$$v_t = P v_{t-1} + \varepsilon_t, \quad (16)$$

where

$$P = \begin{bmatrix} \rho_a & 0 & 0 & 0 \\ 0 & \rho_e & 0 & 0 \\ 0 & 0 & \rho_z & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

and

$$\varepsilon_t = \begin{bmatrix} \varepsilon_{at} & \varepsilon_{et} & \varepsilon_{zt} & \varepsilon_{rt} \end{bmatrix}'.$$

Rewrite (14) as

$$f_t^0 = A^{-1} B s_t^0 + A^{-1} C v_t.$$

When substituted into (15), this last result yields

$$(D + FA^{-1}B)E_t s_{t+1}^0 + FA^{-1}CPv_t = (G + HA^{-1}B)s_t^0 + (J + HA^{-1}C)v_t$$

or, more simply,

$$E_t s_{t+1}^0 = Ks_t^0 + Lv_t, \tag{17}$$

where

$$K = (D + FA^{-1}B)^{-1}(G + HA^{-1}B)$$

and

$$L = (D + FA^{-1}B)^{-1}(J + HA^{-1}C - FA^{-1}CP).$$

If the  $7 \times 7$  matrix  $K$  has five eigenvalues inside the unit circle and two eigenvalues outside the unit circle, then the system has a unique solution. If  $K$  has more than two eigenvalues outside the unit circle, then the system has no solution. If  $K$  has less than two eigenvalues outside the unit circle, then the system has multiple solutions. For details, see Blanchard and Kahn (1980).

**Blanchard, O. and C.M. Kahn (1980), "The solution of linear difference models under rational expectations", *Econometrica*, 48(5), 1305-1311.**

Assuming from now on that there are exactly two eigenvalues outside the unit circle, write  $K$  as

$$K = M^{-1}NM,$$

where

$$N = \begin{bmatrix} N_1 & 0 \\ 0 & N_2 \end{bmatrix}$$

and

$$M = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix}.$$

The diagonal elements of  $N$  are the eigenvalues of  $K$ , with those in the  $5 \times 5$  matrix  $N_1$  inside the unit circle and those in the  $2 \times 2$  matrix  $N_2$  outside the unit circle. The columns of  $M^{-1}$  are the eigenvectors of  $K$ ;  $M_{11}$  is  $5 \times 5$ ,  $M_{12}$  is  $5 \times 2$ ,  $M_{21}$  is  $2 \times 5$ , and  $M_{22}$  is  $2 \times 2$ . In addition, let

$$L = \begin{bmatrix} L_1 \\ L_2 \end{bmatrix},$$

where  $L_1$  is  $5 \times 4$  and  $L_2$  is  $2 \times 4$ .



Now (17) can be rewritten as

$$\begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} E_t s_{t+1}^0 = \begin{bmatrix} N_1 & 0 \\ 0 & N_2 \end{bmatrix} \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} s_t^0 + \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} \begin{bmatrix} L_1 \\ L_2 \end{bmatrix} v_t$$

or

$$E_t s_{1t+1}^1 = N_1 s_{1t}^1 + Q_1 v_t \quad (18)$$

and

$$E_t s_{2t+1}^1 = N_2 s_{2t}^1 + Q_2 v_t, \quad (19)$$

where

$$s_{1t}^1 = M_{11} \begin{bmatrix} \hat{y}_{t-1} \\ \hat{m}_{t-1} \\ \hat{\pi}_{t-1} \\ \hat{r}_{t-1} \\ \hat{\mu}_{t-1} \end{bmatrix} + M_{12} \begin{bmatrix} \hat{y}_t \\ \hat{\pi}_t \end{bmatrix}, \quad (20)$$

$$s_{2t}^1 = M_{21} \begin{bmatrix} \hat{y}_{t-1} \\ \hat{m}_{t-1} \\ \hat{\pi}_{t-1} \\ \hat{r}_{t-1} \\ \hat{\mu}_{t-1} \end{bmatrix} + M_{22} \begin{bmatrix} \hat{y}_t \\ \hat{\pi}_t \end{bmatrix}, \quad (21)$$

$$Q_1 = M_{11}L_1 + M_{12}L_2,$$

and

$$Q_2 = M_{21}L_1 + M_{22}L_2.$$

Since the eigenvalues in  $N_2$  lie outside the unit circle, (19) can be solved forward to obtain

$$s_{2t}^1 = -N_2^{-1} R v_t,$$

where the  $2 \times 4$  matrix  $R$  is given by

$$\begin{aligned} \text{vec}(R) &= \text{vec} \sum_{j=0}^{\infty} N_2^{-j} Q_2 P^j = \sum_{j=0}^{\infty} \text{vec}(N_2^{-j} Q_2 P^j) \\ &= \sum_{j=0}^{\infty} [P^j \otimes (N_2^{-1})^j] \text{vec}(Q_2) = \sum_{j=0}^{\infty} [P \otimes N_2^{-1}]^j \text{vec}(Q_2) \\ &= \left[ I_{(8 \times 8)} - P \otimes N_2^{-1} \right]^{-1} \text{vec}(Q_2) \end{aligned}$$

Use this result, along with (21), to solve for

$$\begin{bmatrix} \hat{y}_t \\ \hat{\pi}_t \end{bmatrix} = S_1 \begin{bmatrix} \hat{y}_{t-1} \\ \hat{m}_{t-1} \\ \hat{\pi}_{t-1} \\ \hat{r}_{t-1} \\ \hat{\mu}_{t-1} \end{bmatrix} + S_2 v_t, \quad (22)$$

where

$$S_1 = -M_{22}^{-1} M_{21}$$

and

$$S_2 = -M_{22}^{-1} N_2^{-1} R.$$

Equation (20) now provides a solution for  $s_{1t}^1$ :

$$s_{1t}^1 = (M_{11} + M_{12}S_1) \begin{bmatrix} \hat{y}_{t-1} \\ \hat{m}_{t-1} \\ \hat{\pi}_{t-1} \\ \hat{r}_{t-1} \\ \hat{\mu}_{t-1} \end{bmatrix} + M_{12}S_2v_t.$$

Substitute this result into (18) to obtain

$$\begin{bmatrix} \hat{y}_t \\ \hat{m}_t \\ \hat{\pi}_t \\ \hat{r}_t \\ \hat{\mu}_t \end{bmatrix} = S_3 \begin{bmatrix} \hat{y}_{t-1} \\ \hat{m}_{t-1} \\ \hat{\pi}_{t-1} \\ \hat{r}_{t-1} \\ \hat{\mu}_{t-1} \end{bmatrix} + S_4v_t, \quad (23)$$

where

$$S_3 = (M_{11} + M_{12}S_1)^{-1}N_1(M_{11} + M_{12}S_1)$$

and

$$S_4 = (M_{11} + M_{12}S_1)^{-1}(Q_1 + N_1M_{12}S_2 - M_{12}S_2P).$$

Finally, return to

$$\begin{aligned} f_t^0 &= A^{-1}Bs_t^0 + A^{-1}Cv_t \\ &= A^{-1}B \begin{bmatrix} I_{(5 \times 5)} \\ S_1 \end{bmatrix} \begin{bmatrix} \hat{y}_{t-1} \\ \hat{m}_{t-1} \\ \hat{\pi}_{t-1} \\ \hat{r}_{t-1} \\ \hat{\mu}_{t-1} \end{bmatrix} + A^{-1}B \begin{bmatrix} 0_{(5 \times 4)} \\ S_2 \end{bmatrix} v_t + A^{-1}Cv_t, \end{aligned}$$

which can be written more simply as

$$f_t^0 = S_5 \hat{m}_{t-1} + S_6 v_t, \tag{24}$$

where

$$S_5 = A^{-1}B \begin{bmatrix} I_{(5 \times 5)} \\ S_1 \end{bmatrix}$$

and

$$S_6 = A^{-1}B \begin{bmatrix} 0_{(5 \times 4)} \\ S_2 \end{bmatrix} + A^{-1}C.$$

Equations (16) and (22)-(24) provide the model's solution:

$$s_{t+1} = \Pi s_t + W \varepsilon_{t+1} \quad (25)$$

and

$$f_t = U s_t, \quad (26)$$

where

$$s_t = \left[ \hat{y}_{t-1} \quad \hat{m}_{t-1} \quad \hat{\pi}_{t-1} \quad \hat{r}_{t-1} \quad \hat{\mu}_{t-1} \quad \hat{a}_t \quad \hat{e}_t \quad \hat{z}_t \quad \varepsilon_{Rt} \right]',$$

$$f_t = \left[ \hat{m}_t \quad \hat{r}_t \quad \hat{\mu}_t \quad \hat{y}_t \quad \hat{\pi}_t \right]',$$

$$\varepsilon_t = \left[ \varepsilon_{at} \quad \varepsilon_{et} \quad \varepsilon_{zt} \quad \varepsilon_{rt} \right]',$$

$$\Pi = \begin{bmatrix} S_3 & S_4 \\ 0_{(4 \times 5)} & P \end{bmatrix},$$

$$W = \begin{bmatrix} 0_{(5 \times 4)} \\ I_{(4 \times 4)} \end{bmatrix},$$

and

$$U = \begin{bmatrix} S_5 & S_6 \\ S_1 & S_2 \end{bmatrix}.$$



